

Withstanding the Pressure

How to pre-stress your press-pack power semiconductors

To achieve optimum performance of press-pack power semiconductors, they must be mechanically clamped in a precise manner. This article explains a technique to verify that the pressure distribution is homogenous and the magnitude is appropriate during the design of the assembly.

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Press-pack high power semiconductors are in many applications very powerful components in controlling electrical power. To utilize their full potential, a proper mechanical design of the complete assembly, including press-pack high power semiconductors, heat sinks, bus bars and other components, is crucial. This article addresses some important issues for the mechanical design and the assembly work for stacks using press-pack high power semiconductors and also shows how the pressure distribution can be verified using Pressurex[®] film.

Interface properties

The current and heat conducting interfaces should be designed to retain good conduction properties throughout the equipment lifetime. This is accomplished by creating a sufficient number of stable metal-to-metal connections, referred to as “a-spots” in contact theory, which can efficiently conduct current from the semiconductor through the heat sink to the bus bars. These a-spots must be maintained during high stress conditions such as load cycling, vibration and chemical contamination such as exposure to sulphur gases. To achieve this, care must be taken in choosing the right materials for the components, which must be coated properly and have the right surface finish. Since the most critical interface is between the press-pack high power semiconductor and the heat sink, we will focus on this interface

Surface finish and treatment are crucial processes for optimal heat and current conduction over the device and heat sink interface. Press-pack high power semiconductors usually have a surface roughness Ra about 0.8 μm and flatness below 10 or 15 μm depending on pole piece size. It is recommended that the heat-sink surfaces have the same flatness and roughness as the press-pack high power semiconductor measured

on the surface where the device is to be mounted.

The use of heat sinks with a good quality plating of nickel or silver is recommended... Bare copper or aluminum is not recommended due to corrosion that rapidly deteriorates the contact surfaces. Although nickel and silver do corrode, the nickel and silver oxide do not deteriorate the interface to the same extent as aluminum oxide. Often press-pack high power semiconductors have pole pieces of copper with a nickel-plating of approximately 5 μm . For nickel-plated devices it is recommended to use the same plating thickness on the heat-sink area that is in contact with the device. For applications with hard component stress, it is recommended to use chemical plating when the semiconductor is electrolytically plated or vice versa.

Mechanical design

The clamping must be carefully designed to ensure that the device is clamped with the right force and it must also allow homogeneous pressure distribution over the whole contact surface of the device. Uneven pressure will lead to deformation of the housing and internal stress between the different layers inside the device, causing it to fail prematurely during load cycling. Designing for pressure uniformity is not always easy, and the complexity should not be underestimated. Simple solutions, such as clamping the device between two rectangular plates by bolting down the corners will result in poor reliability.

Ideally, the mounting force should be applied from a single point above the centre of the device. Our recommendation is that the centre of the force is within 2 mm from the centre of the device, and at a minimum distance equal to half the pole-piece diameter of the

device measured from the device surface, as shown in Figure 1, to achieve a good pressure uniformity considering the “90° force cone”. A spherical cup between the mounting clamp and the pressure spreader above the heat-sink can act as this single point of force and ensures that the force from the mounting clamp is transferred symmetrically to the device. It also allows parts within the stack to adapt to inherently present non-parallelisms. There will always be inherent non-parallelisms in a stack since it is not possible to manufacture heat sinks and press-pack high power semiconductors with perfectly parallel surfaces, but the non-parallelisms should be reduced as much as possible. The non-parallelism between the anode and cathode pole pieces is normally $\leq 100 \mu\text{m}$ for devices with a pole piece diameter $\leq 50 \text{ mm}$ and $\leq 150 \mu\text{m}$ for devices with a pole piece diameter $> 50 \text{ mm}$.

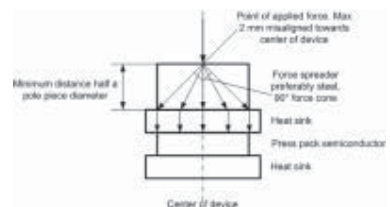


Figure 1: Force spread cone.

The components and the clamp design must be chosen to withstand temperature levels and forces caused by mechanical expansions and contractions due to temperature changes that occur during working conditions, to prevent damage over the whole equipment lifetime. The design must also allow for temperature expansion and contraction without large changes in force and pressure distribution on the press-pack high power semiconductor.

Press-pack high power semiconductors, whether parallel or anti-parallel connected,

further investigation is normally needed. If the result is bad, the next step is to apply a pressure film on the other interfaces in the stack, as between the heat sink and bus bar or between the heat sink and force spreader. This gives the complete picture of the force distribution within the stack, thus enabling tracking of the weak point in the system that needs to be improved to get good force distribution on the power semiconductor.

Figures 5 and 6 show two samples from pressure distribution measurements on IGCT's with Pressurex® film. Figure 5 shows good pressure distribution and figure 6 shows poor pressure distribution, with a large area of the device having too low pressure and some areas having to high pressure.

Seldom are the cases clearcut. There are unfortunately no simple rules that predict whether a mechanical design will be good enough for its intended purpose. Experience is normally the only way to determine if a design is good enough for its purpose or not.



Figure 5: Good pressure distribution

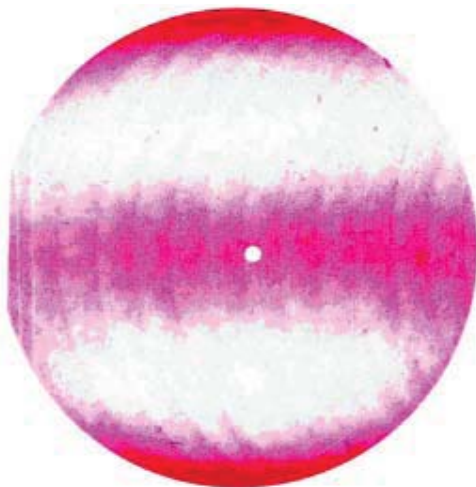


Figure 6: Poor pressure distribution

Advanced verification of the pressure distribution

In addition to the simple visual investigation of the pressure film, there are more sophisticated analysis tools available such as the Topaq Tactile Force Analysis System®.

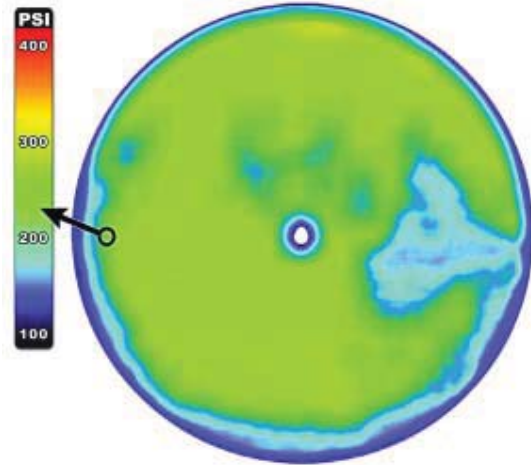


Figure 7: Analyzing the pressure distribution in Figure 5 with the Topaq Tactile Force Analysis System

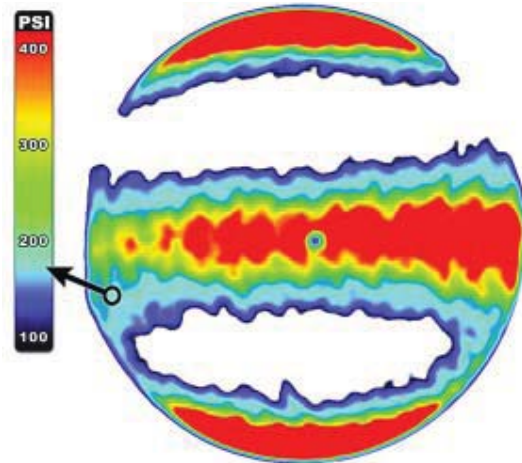


Figure 8: Analyzing the pressure distribution in Figure 6 with the Topaq Tactile Force Analysis System

With this tool, the various shades of red that show pressure distribution on the film are presented in a wider range of colors, giving a highly-detailed statistical picture of the pressure distribution. When analyzing the examples from figures 5 and 6, we get the following results:

As can be seen, the homogeneity in figure 5 is not as good as first thought, although it is for practical purposes good enough. For figure 8, we see that the spread in pressure distribution is large and that further measures are needed to improve the situation before the equipment using this semiconductor goes into operation.

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